Impact response of composites with an embedded battery

Koranat (Bright) Pattarakunnan s3567979

Supervisory team: Distinguished Prof. Adrian Mouritz Dr. Joel Galos Dr. Adam Best (CSIRO) Dr. Louis Kyratzis (CSIRO)













Outlines

- 1) Motivation & background
- 2) Composites with embedded batteries
- 3) Manufacturing methods
- 4) Impact response
- 5) Risks to health and safety
- 6) Conclusion







Motivation & Background

Integrating load-bearing composite structure and electrical energy storage devices leads to a reduction in empty mass (i.e. battery housing/casing). Hence, *specific electrical energy capacity can be improved.*



Tesla Model S battery pack https://qnovo.com/peek-inside-the-battery-of-a-tesla-model-s/ https://www.teslarati.com/tesla-model-s-weight/

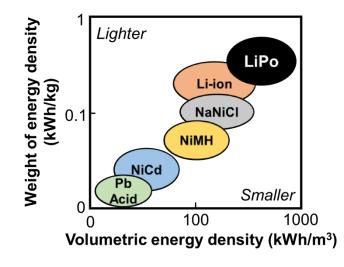
The total battery pack weight (~600 kg) corresponds to 30% of the overall vehicle mass.

Approaches to achieve multifunctional composites:

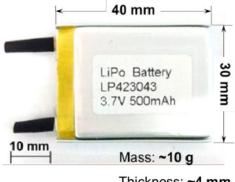
- 1) Composites with embedded batteries
- 2) Structural power composites

Composites with embedded batteries

Lithium-ion batteries are embedded into fibre reinforced composites to construct *multifunctional energy storage composites*.



⁽a) Gravimetric and volumetric of various battery chemistries Adapted from Manzetti et al., 2015



Thickness: ~4 mm

(b) Pouch batteries LiPol Battery Co. Ltd, China.

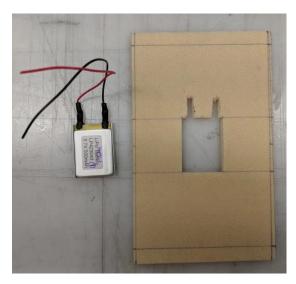
Manufacturing methods

- 1) CFRP laminates: Vacuum assisted resin infusion
- 2) CFRP/PVC foam sandwich composites: Wet hand lay-up + Vacuum bagging



(a) Cut-outs in the middle 18 plies of CFRP





(b) Cut-out in the foam core



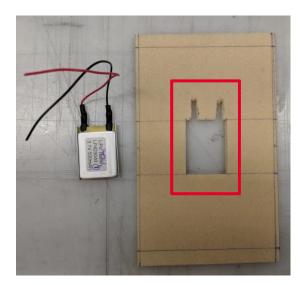
Manufacturing methods

- 1) CFRP laminates: Vacuum assisted resin infusion
- 2) CFRP/PVC foam sandwich composites: Wet hand lay-up + Vacuum bagging



(a) Cut-outs in the middle 18 plies of CFRP





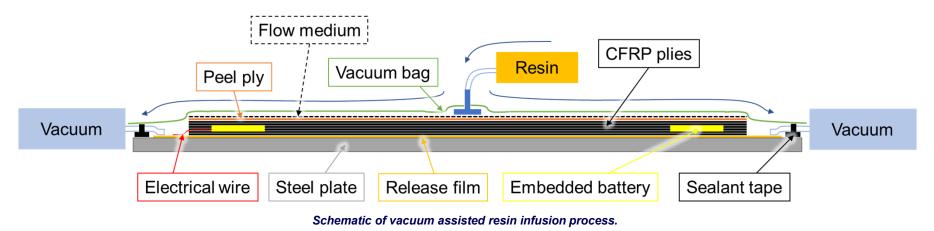
(b) Cut-out in the foam core





Manufacturing methods

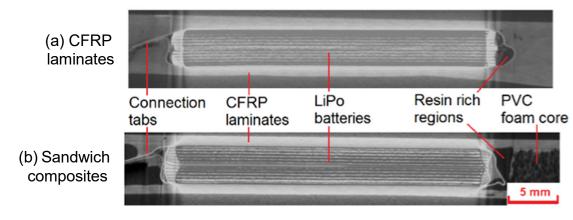
Both composites were cured under *vacuum bag* (~1 *atm*) and *room temperature* (~20 °C) for at least 24 hours. *No post cure* that usually applies excessive pressure and heat was conducted to avoid damaging the embedded batteries.





X-ray CT images

- Embedded battery adhered well to surrounding composites
- Embedded battery caused no damage to the surrounding composites
- Embedded battery was not damaged from the composites manufacturing methods

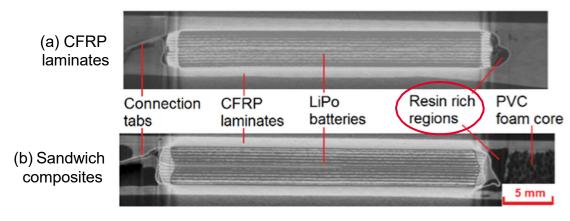




X-ray CT images of embedded battery

X-ray CT images

- Embedded battery adhered well to surrounding composites
- Embedded battery caused no damage to the surrounding composites
- Embedded battery was not damaged from the composites manufacturing methods



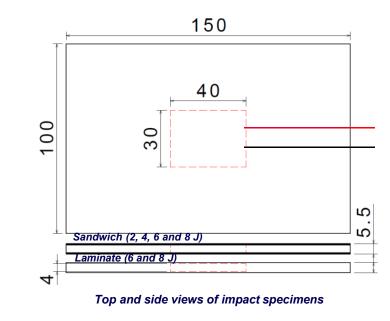


X-ray CT images of embedded battery

Impact samples

Standard test method for measuring the damage resistance of a fibre-reinforced polymer matrix composite to a drop-weight impact event (ASTM D7136) & Standard test method for compressive residual strength properties of damaged polymer matrix composite plates (ASTM D7137).

- A minimum of 5 samples for both specimen types



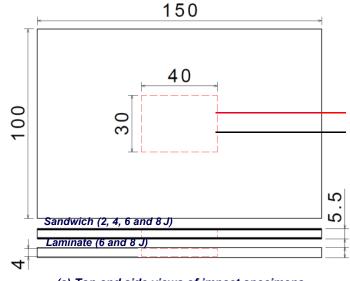




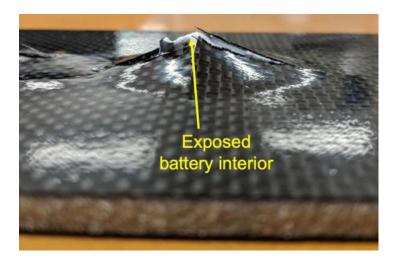
Impact samples

Standard test method for measuring the damage resistance of a fibre-reinforced polymer matrix composite to a drop-weight impact event (ASTM D7136) & Standard test method for compressive residual strength properties of damaged polymer matrix composite plates (ASTM D7137).

- A minimum of 5 samples for both specimen types



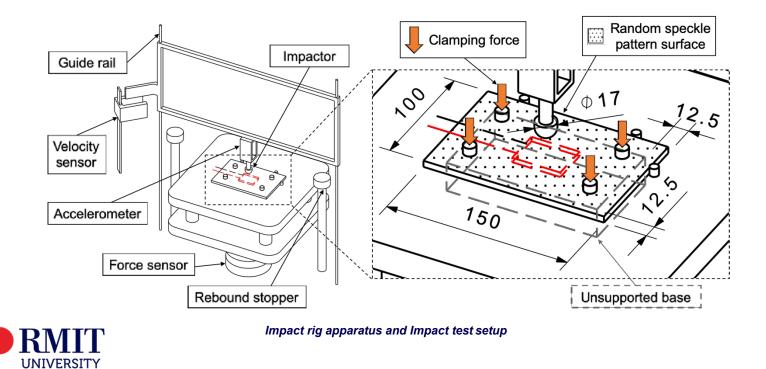
(a) Top and side views of impact specimens



(b) Impact damage of sandwich composites subjected to 10 J impact

Impact rig

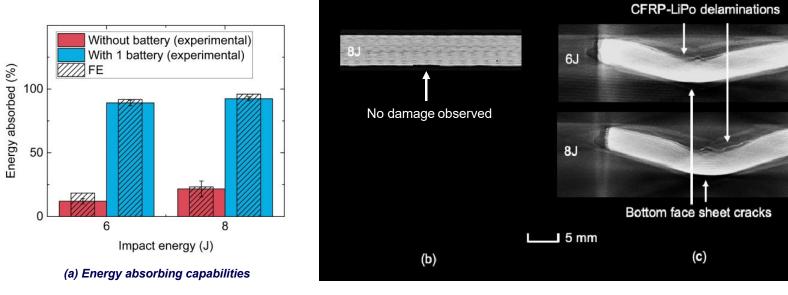
Samples were impacted once and then compressed in out-of-plane direction.



12

Energy absorbing capabilities & impact damages – CFRP laminates with an embedded battery

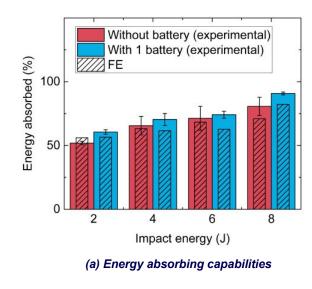
Embedded battery significantly increase energy absorbing capabilities and change damage mechanisms of CFRP laminates.

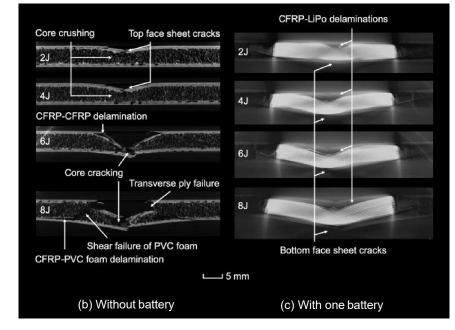


X-ray CT images showing impact damages

Energy absorbing capabilities & impact damages – CFRP/PVC sandwich composites with an embedded battery

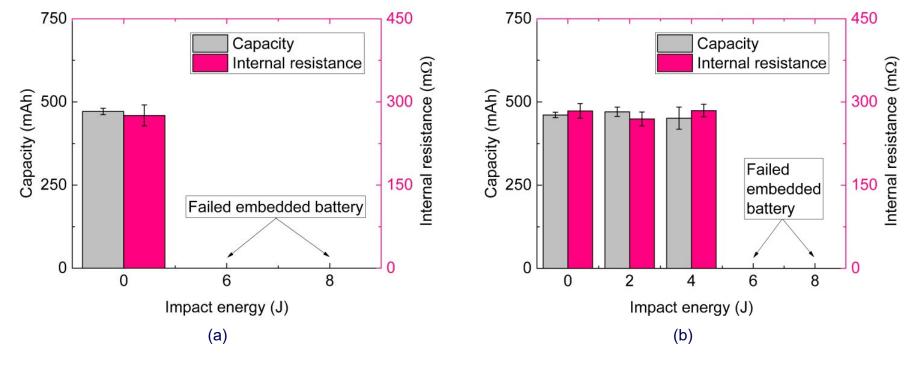
Embedded battery changed damage mechanisms of sandwich composites but did not significantly affect their energy absorbing capabilities.





X-ray CT images showing impact damages

Electrical properties





Electrical properties of (a) CFRP laminates and (b) sandwich composites before and after impact event

Risks to health and safety

- Higher impact energy (> 8 J), could possibly cause sudden fire and explosion after the crash
- Fire would emit toxic gases such as Carbon Monoxide (CO) and carcinogenic Hydrogen Fluoride (HF)







Conclusion

- Composites with embedded batteries can be manufactured by composites manufacturing methods
- Embedded battery significantly changed CFRP laminates impact responses
- LiPo battery can be a potential energy absorbing material
- Impact energy of up to 8 J did not cause sudden fire and explosion
- Impact energy of higher than 8 J could possibly cause sudden fire and explosion which results in an emission of toxic gases such as CO and HF.





Publications

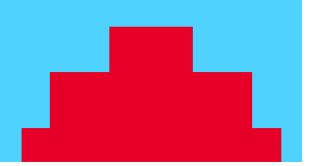
- **K. Pattarakunnan**, J. Galos, and A. P. Mouritz, "A review of energy storage composite structures with embedded lithium-ion batteries," *Proceedings of the 22nd International Conference on Composite Materials, Melbourne, Australia, 11-16 August, 2019.*
- **K. Pattarakunnan**, J. Galos, R. Das, and A. P. Mouritz, "Tensile properties of multifunctional composites embedded with lithium-ion polymer batteries," *Composites Part A: Applied Science and Manufacturing*, p. 105966, 2020.





Thank you







Backup slides





Specimens fabrication

- Material system
 - 200 g/m² plain woven T300 carbon fabric (AC220127 supplied by Colan Ltd.)
 - 4-mm H100 Divinycell PVC foam (100 kg/m³)
 - 500 mAh and 3.7 V LiPo battery (LP423043 from LiPol Battery Co. Ltd, China)
 - Low-temperature cure bisphenol-A epoxy resin (West system)
 - One-part 206 slow hardener
 - Five-part 105 resin
 - Araldite 420 A/B adhesive
 - Plain woven glass fibre
- Wet hand layup for sandwich specimens
- Resin infusion for laminate specimens





Impact modelling

- Sandwich composite (150mm x 100mm x 5.5mm)
 - CFRP facesheets (Colan 198gsm woven plain weave)
 - Foam core (H100 Divinycell PVC foam)
 - Epoxy (West system 105 Resin + 206 Slow hardener)
 - Battery (LiPol 500mAh LiPo battery)
- Steel impactor





CFRP modelling approach (1/2)

- Each ply is modelled individually as continuum shell (SC8R)
- Built-in VUMAT for woven fabric reinforced composites (ABQ_PLY_FABRIC) is selected to introduce plasticity and damage
 - Applicable for only shell, plane stress, and membrane elements





CFRP modelling approach (2/2)

26 user material constants must be specified for this subroutine

Young's moduli in fiber 1- and 2-directions

 $- E_{1+/-}, E_{2+/-}$

Poisson's ratio

 $- \nu_{12+}, \nu_{12-}$

Shear modulus

 $- G_{12}$

Shear stress at the onset of shear damage

-S

• Tensile and compressive strength along fiber directions

 $- X_{1+/-}, X_{2+/-}$

Shear equation parameters

 $-\alpha^{12}, d^{12}_{max}$

- Energy per unit area for tensile and compressive fracture along fiber directions $-G_{f}^{1+/-}, G_{f}^{2+/-}$
- Shear plasticity coefficients

 σ_{y0}, C, p

Controls for material point failure

- IDelFlag, d_{\max} , \mathcal{B}^{l}_{\max} , \mathcal{E}_{\max} , \mathcal{E}_{\min}

Foam modelling approach

- A foam core is modelled as 3D solid element (C3D8R)
- Crushable foam plasticity + Crushable foam hardening is used to introduce plasticity
 - Isotropic material must only be used in this criteria





Epoxy modelling approach (1/2)

- Epoxy is modelled as cohesive interaction between each of the CFRP plies and between CFRP plies and foam core
 - Damage initiation criteria: Quadratic stress criterion >> Damage is assumed to initiate when a sum of ratio in below formula reaches 1

$$\left(\frac{\left\langle t_n \right\rangle}{t_n^{\max}}\right)^2 + \left(\frac{t_s}{t_s^{\max}}\right)^2 + \left(\frac{t_t}{t_t^{\max}}\right)^2 = 1$$

- *tn*: normal contact stress in the pure normal mode
- *ts*: shear contact stress along the first shear direction
- *tt*: shear contact stress along the second shear direction



alle.

Epoxy modelling approach (2/2)

The damage evolution is governed by fracture energy from Benzeggagh-Kenane (BK) criteria as presented below

$$G_{IC} + \left(G_{IIC} - G_{IC}\right) \left(\frac{G_{shear}}{G_T}\right)^{\eta} = G_{TC}$$

where $G_{shear} = G_{II} + G_{III}$ $G_T = G_I + G_{shear}$



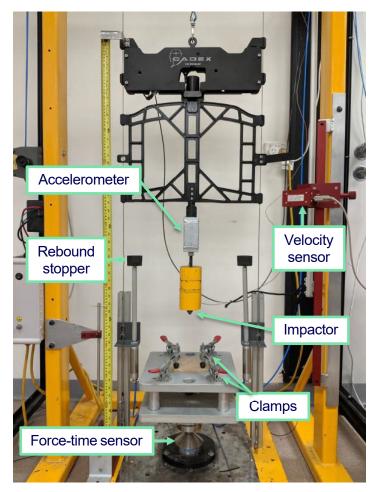
Contact algorithm

- General contact (explicit) is used
 - Specify hard contact to prevent elements penetration
 - Specify coefficient of friction to be 0.2
 - Specify contacts between plies and plies, and plies and core as cohesive interaction





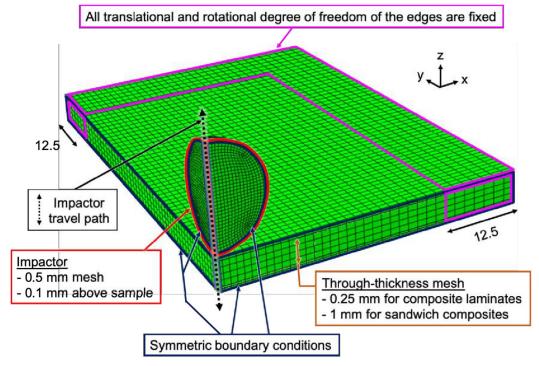
RMIT Classification: Trusted







FE model – Impact test





FE model of the impact test showing meshing strategy and boundary condition

Electrical properties before and after impact

Impact energy (J)	Capacity (mAh)	Internal resistance (mΩ)
CFRP laminate		
0	471.3 ± 9.6	275.6 ± 19.0
6	~ 0	α
8	~ 0	α
Sandwich composite		
0	460.8 ± 8.4	283.8 ± 13.1
2	470.3 ± 14.0	269.3 ± 12.6
4	451.0 ± 33.4	284.5 ± 11.3
6	~ 0	α
8	~ 0	α

Electrical properties of embedded batteries subjected to impact loading



alle i